Introduction into design engineering week 5

Dr. Yukari AOKI

Question 2: knowing that P=160 EN, determine the average normal stress at the midsection of (a) rod AB, (b) rod BC 75 mm 50 mm 120 kN B 160FN Ana 120 kN ABC 750 m 1000 mn AAB = 1963.5 mm2 OLAB = P = 160KM = 81.5 MPa ... + average normal stress at rod AB (tension) 75 mm ABC = 44/2 9mm2 PBC +120+120 120 kN B = (60 Pec 160 4 OBC - PBC ABC Pec= 160-240 120 kN ABC -80KM -80km 1000 mm nm 4417.9 mm2 = -18.1 MPa - the average normal stress or rod BC. (compression

Shearing stress

- The internal forces and the corresponding stresses discussed in the previous sessions were normal to the section considered.
- A very different type of stress is obtained when transverse forces
 P and P' are applied to a member AB (Fig.1.15)





• Passing a section at C between the points of application of the two forces (Fig.1.16*a*), it is obtained that the diagram of portion *AC* shown in Fig.1.16*b*.

• It is concluded that the internal forces must exist in the plane of the section, and that their resultant is equal to *P*.

• These elementary internal forces are called *shearing forces*, and the magnitude *P* of their resultant is the *shear* in the section.

POD

- Dividing the shear *P* by the area *A* of the cross section, it is obtained the *average shearing stress* in the section.
- Denoting the <u>shearing stress</u> by the Greek letter τ (tau), it is written as;

(1.8)

$$\tau_{\rm ave} = \frac{P}{A}$$



- It should be emphasized that the value obtained is an *average value of the shearing stress* over the entire section.
- Contrary to what we said earlier for normal stresses, the distribution of shearing stresses across the section cannot be assumed uniform.
- The actual value τ of the shearing stress varies from zero at the surface of the member to a maximum value τ_{max} that may be much larger than the average value τ_{ave} .

• Shearing stresses are commonly found in bolts, pins, and rivets used to connect various structural members and machine components (Fig 1.17).



• Consider the two plates A and B, which are connected by a bolt CD (Fig.1.18).



- If the plates are subjected to tension forces of magnitude *F*, stresses will develop in the section of bolt corresponding to the plane *EE*'.
- Drawing the diagram of the bolt and of the portion located above the plane *EE*' (Fig.1.19), it is concluded that the shear P in the section is equal to *F*.



TANE = P (1.8)

The average shearing stress in the section is obtained, according to formula (1.8), by dividing the shear
 P=*F* by the area A of the cross section.

$$\tau_{\rm ave} = \frac{P}{A} = \frac{F}{A}$$

(1.9)

- The bolt we have just considered is said to be in *single shear*.
- Different loading situations may arise, however.

- For example, if splice plates *C* and *D* are used to connect plates *A* and *B* (Fig.1.20), shear will take place in bolt *HJ* in each of the two planes *KK*' and *LL*' (and similarly in bolt *EG*).
- The bolts are said to be in *double shear*.



To determine the average shearing stress in each plane, it can be drawn <u>free-body diagrams</u> of bolt *HJ* and of the portion of bolt located between the two planes (Fig.1.21).



Fig. 1.21

(a)

Fig. 1.20

Observing that the shear *P* in each of the sections is *P=F/2*, it is concluded that the average shearing stress is

$$\tau_{\rm ave} = \frac{P}{A} = \frac{F/2}{A} = \frac{F}{2A}$$
 (1.10)

Bearing stress in connections

- Bolts, pins, and rivets create stresses in the members they connect, along the *bearing surface*, or surface of contact.
- For example, consider again the two plates *A* and *B* connected by a bolt *CD* that we have discussed in the preceding section (Fig.1.18).





The bolt exerts on plate *A* a force *P* equal and opposite to the force *F* exerted by the plate on the bolt (Fig.1.22).



• The force *P* represents the resultant of elementary forces distributed on the inside surface of a half-cylinder of diameter *d* and of length *t* equal to the thickness of the plate.

Since the distribution of these forces – and of the corresponding stresses – is quite complicated, one uses in practice an average nominal value σ_b of the stress, called *the bearing stress*, obtained by dividing the load *P* by the area of the rectangle representing the projection of the bolt on the plate section to (Fig.1.23).



Fig. 1.23

• Since this area is equal to *td*, where *t* is the plate thickness and d the diameter of the bolt, we can have

$$\sigma_b = \frac{P}{A} = \frac{P}{td}$$



(1.11)

Design

- The engineer's role is not limited to the analysis of existing structures and machines subjected to given loading conditions.
- Of even greater importance to the engineer is <u>the design of new structures</u> <u>and machines</u>, that is, the selection of appropriate components to perform a given task.

Example of Design using Fig.1.1

- Now let's assume that <u>aluminum</u> with an allowable stress σ_{all} =100MPa is to be used.
- Since the force in rod *BC* will still be

 $P=F_{BC}=50kN$ under the given loading applied,





Since the value obtained for *σ* (=159 MPa) is bigger than the value *σ_{all}* (=100 Mpa) of the allowable stress in the aluminum used, it must be re-designed the *Area of rod BC* by the following equation;

 $=\frac{50\times10^3\,\mathrm{N}}{100\times10^6\,\mathrm{Pa}}$

 $= 500 \times 10^{-6} \,\mathrm{m}^2$

 $\sigma_{
m all}$

Toll = a² • Since $\underline{A + \pi r^2}$

$$r = \sqrt{\frac{A}{\pi}} = \sqrt{\frac{500 \times 10^{-6} \text{ m}^2}{\pi}} = 12.62 \times 10^{-3} \text{ m} = 12.62 \text{ mm}}$$

$$We \text{ bclass}$$

$$d = 2r = 25.2 \text{ mm}$$

 It is concluded that an *aluminum rod* <u>26 mm or</u> <u>more in diameter</u> will be adequate.



Two solid cylindrical rods *AB* and *BC* are welded together at *B* and loaded as shown.

Knowing that the average normal stress must not exceed 175 MPa in rod AB and 150 MPa in rod BC, determine the o_1 smallest allowable values of d_1 and d_2 .

