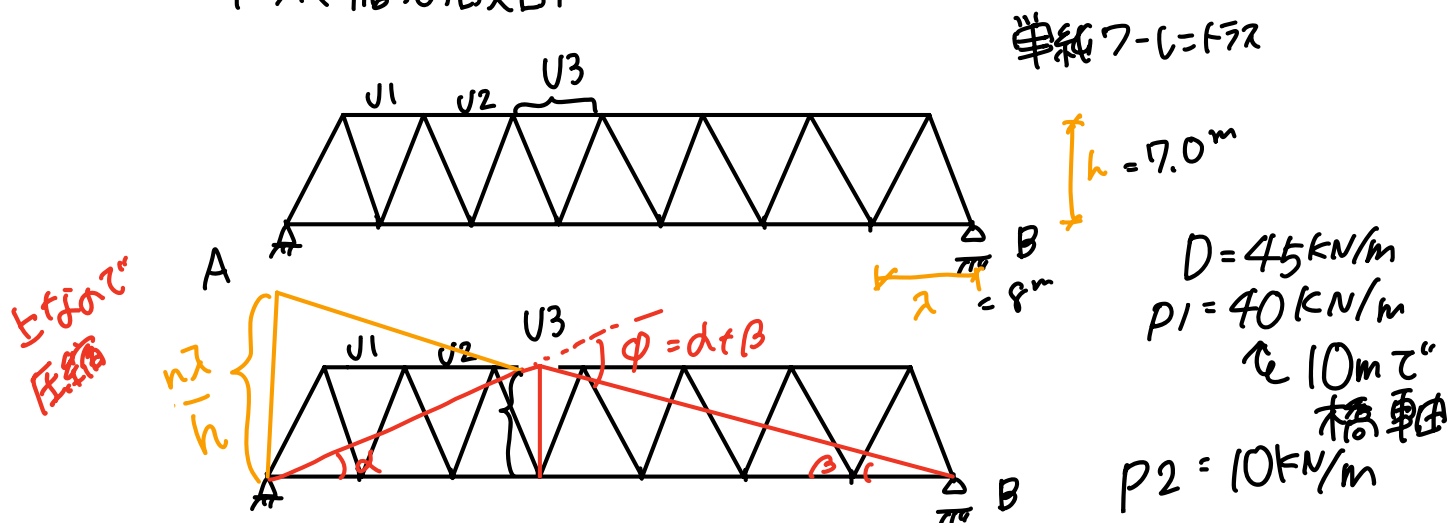
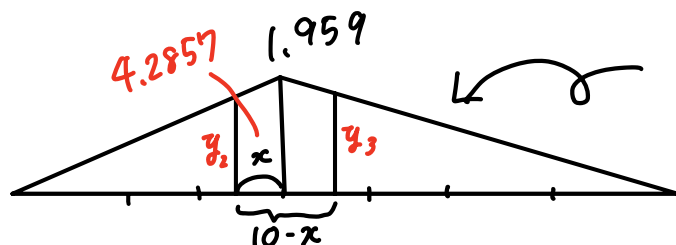


第15回 鋼構造

トラス橋の設計



$$\frac{3\lambda}{h} : 7\lambda = y_1 : 4\lambda \quad y_1 = 4\lambda \cdot \frac{3\lambda}{h} \cdot \frac{1}{7\lambda} = \frac{12\lambda}{7h} = \frac{12 \cdot 8}{7 \cdot 7} = 1.959$$



Max $\Rightarrow y_2 = y_3$

$$1.959 : 3\lambda = y_2 : 3\lambda - x \quad \leftarrow \lambda = 8\text{m}$$

$$1.959 : 4\lambda = y_3 : 4\lambda - (10 - x)$$

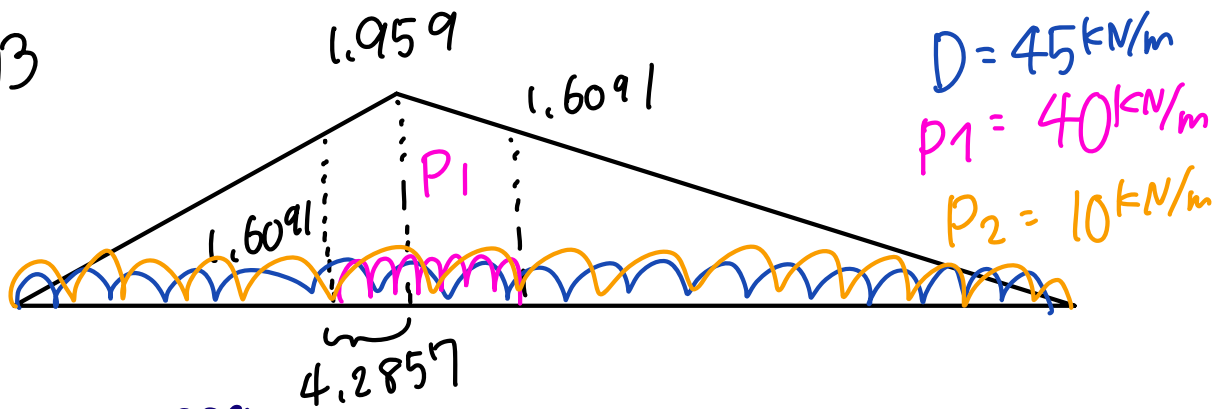
$$y_2 = \frac{(24 - x)}{24} \times 1.959 \quad y_3 = \frac{\{32 - (10 - x)\}}{32} \times 1.959$$

$y_2 = y_3$ として解く.

$x = 4.2857$ この値を y_2, y_3 の式に戻して y_2 と y_3 の値を計算する

$$y_2 = \frac{(24 - 4.2857)}{24} \times 1.959 = 1.6091$$

V3



$$D = \frac{1.959}{7\pi} \times 45 \text{ kN/m} = 2468.34 \text{ kN}$$

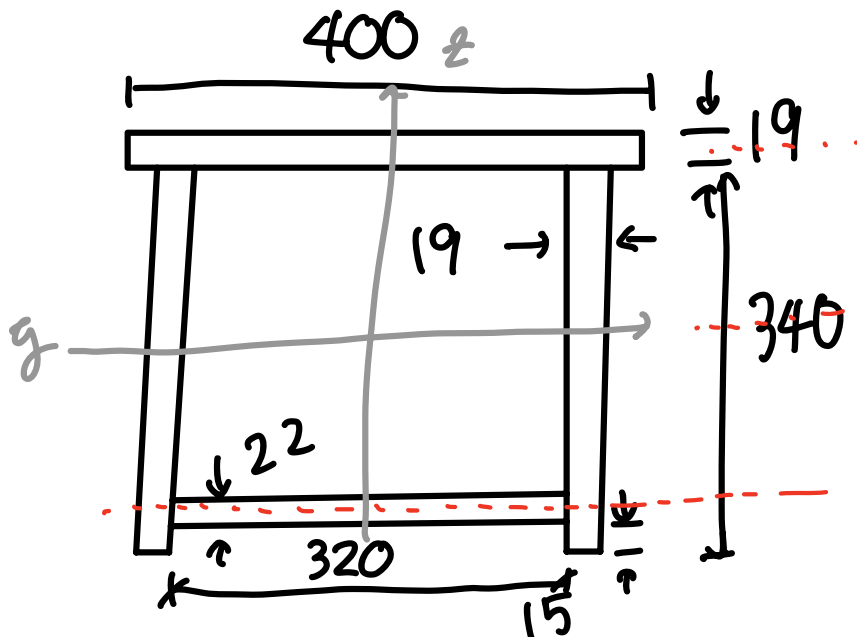
$$NL_{p2} = \frac{1.609}{10} \times 10 \text{ kN/m} = 548.52 \text{ kN}$$

$$NL_{p1} = \frac{1.956}{10} \times 1.609 \times 40 \text{ kN/m} = \left\{ \frac{1.956}{10} + \frac{1.609}{10} \right\} \times 40 \text{ kN/m} = 713.60 \text{ kN}$$

$$\rightarrow \boxed{} \leftarrow D = 2468.34 \text{ kN}$$

$$\rightarrow \boxed{} \leftarrow L = NL_{p1} + NL_{p2} = 713.60 + 548.52 = 1262.12 \text{ kN}$$

SM490Y (降伏応力 355 MPa)



	400×19				I_y
	UFlg	A	y	Ay	Ay ²
$2 \times 346 \times 19$	← 2x Web	7600	-179.5	-1364000	244,874,000
320×22	← LFlg	12920	0	0	124,463,000
		7040	144	1,014000	145,981,000
SUM		27560		-350000	<u>515,318,000</u>

中立軸を修正する 断面一次 / 断面
 Ay / A

$$e = -350000 / 27560 = -12.7 \text{ mm}$$

断面二次モーメントも修正

$$I_y - A \cdot e^2 = 510873000 \text{ mm}^4 \quad \star \text{修正した断面二次}$$

$$\text{有効陸屈長} \Rightarrow l_y = 8000 \text{ mm}$$

$$\text{断面二次半径 } r_y = \sqrt{\frac{I_y}{A}} = \sqrt{\frac{510873000}{27560}} = 136 \text{ mm}$$

$$\text{細長比 } \frac{l_y}{r_y} = \frac{8000 \text{ mm}}{136 \text{ mm}} = 58.8 < 120$$

$$\text{作用応力 } \sigma = \frac{F}{A}$$

$$= \frac{\sigma_{p1} \sigma_{g1} N_D + \sigma_{p2} \sigma_{g2} N_L}{A}$$

$$= \frac{1.0 \times 1.05 (2468.34 \text{ kN} \times 1000) + 1.0 \times 1.25 \times (1262.12 \text{ kN} \times 1000)}{27560}$$

$$= 151.28 \text{ N/mm}^2$$

制限値 σ_{cud}

$$= \underbrace{0.90} \cdot \underbrace{1.0} \cdot \underbrace{0.85} \cdot \underbrace{0.737} \cdot \underbrace{1.0} \cdot \underbrace{355}$$

$$= \underbrace{\beta_1 \beta_2 \Phi}_{\text{I}} \cdot \underbrace{\rho_{\text{cr}g}}_{\text{II}} \cdot \underbrace{\rho_{\text{cr}l}}_{\text{III}} \cdot \underbrace{\sigma_{yk}}_{\text{IV}}$$

E: ヤング率
= 200 GPa

$$\lambda = \frac{1}{\pi} \sqrt{\frac{\sigma_{yk}}{E}} \cdot \frac{l_y}{r_y}$$

$$= \frac{1}{\pi} \sqrt{\frac{355 \text{ N/mm}^2}{200000 \text{ N/mm}^2}} \cdot \frac{8000}{136} = 0.788$$

$$\rho_{\text{cr}g} = \begin{cases} 1.00 & (\lambda \leq 0.2) \\ \star 1.059 - 0.258\lambda - 0.19\lambda^2 & (0.2 \leq \lambda \leq 1.0) \\ 1.427 - 1.039\lambda - 0.223\lambda^2 & (\lambda > 1.0) \end{cases}$$

$$\rho_{\text{cr}g} = 1.059 - 0.258 \cdot (0.788) - 0.19(0.788)^2$$

$$= 0.737$$

$$\sigma_{\text{cud}} = 200.1 \text{ N/mm}^2$$

$$\sigma_{\text{cd}} < \sigma_{\text{cud}}$$

限界状態を満足する

