

プレストレス木箱桁橋のFEMモデル化について

修工12-136 上村哲範

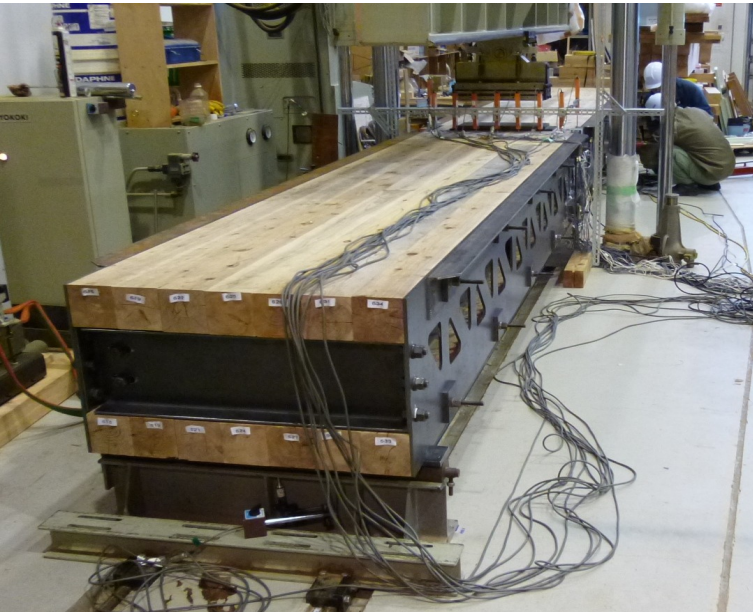
現地製材・組み立て・施工



被災地でも活躍

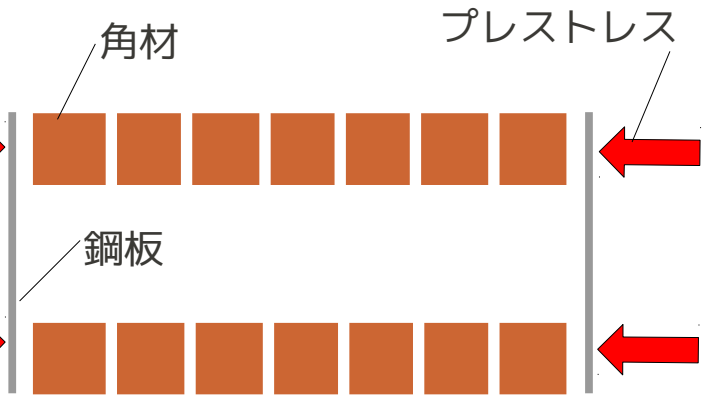
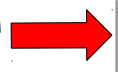
試験体のFEMモデル化

数値解析シミュレーション



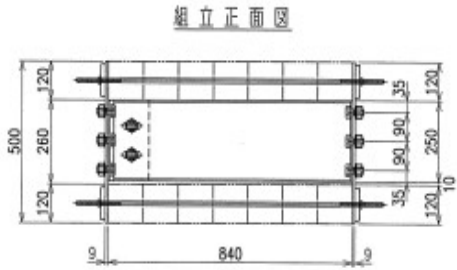
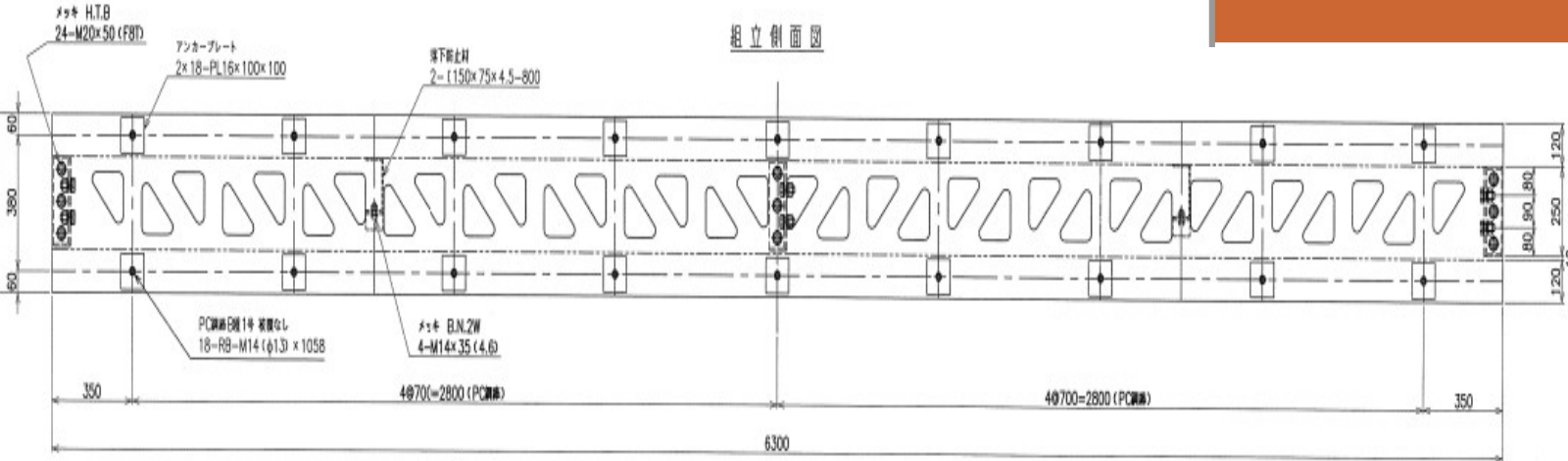
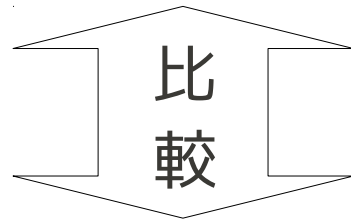
非一体化モデル

モデル化難しい



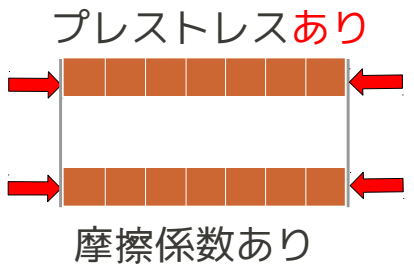
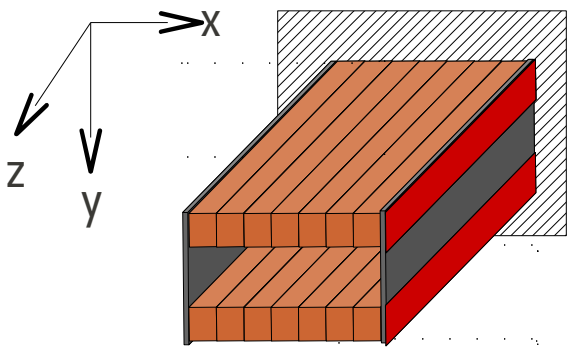
一体化モデル

モデル化簡単



有限要素解析モデル

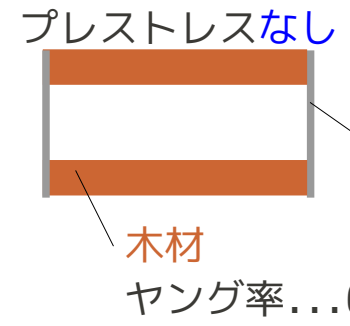
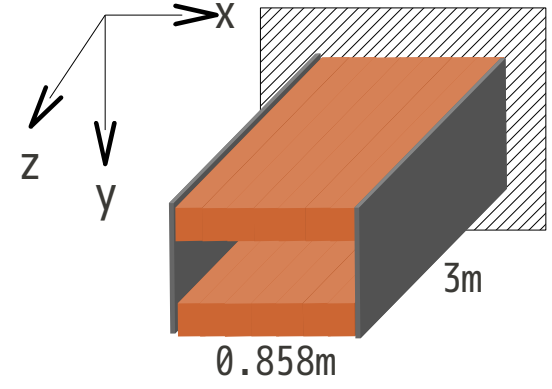
非一体化モデル



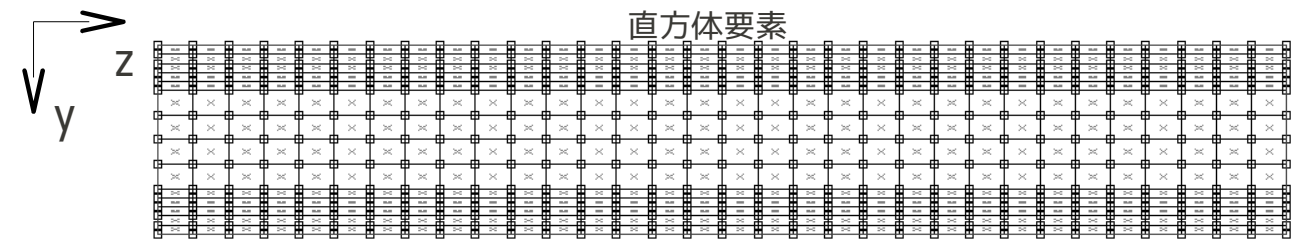
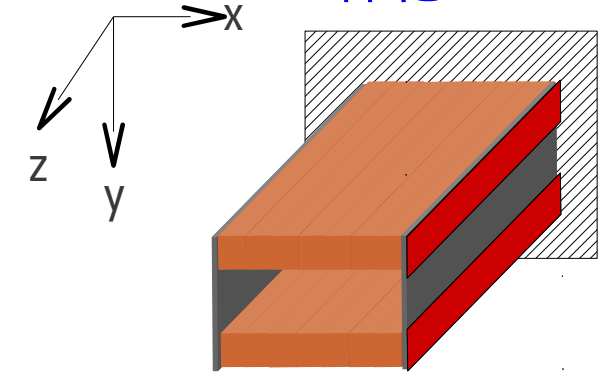
試験体

解析...プレストレス相当の分布外力

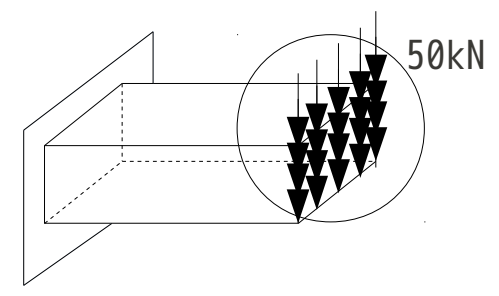
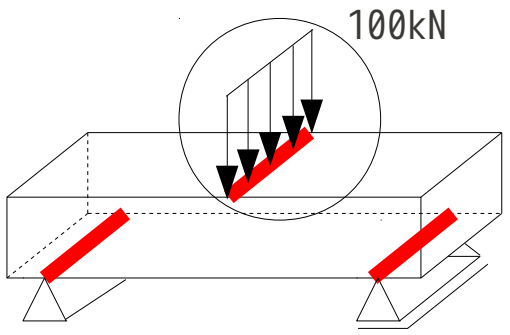
一体化モデル



一体化モデル



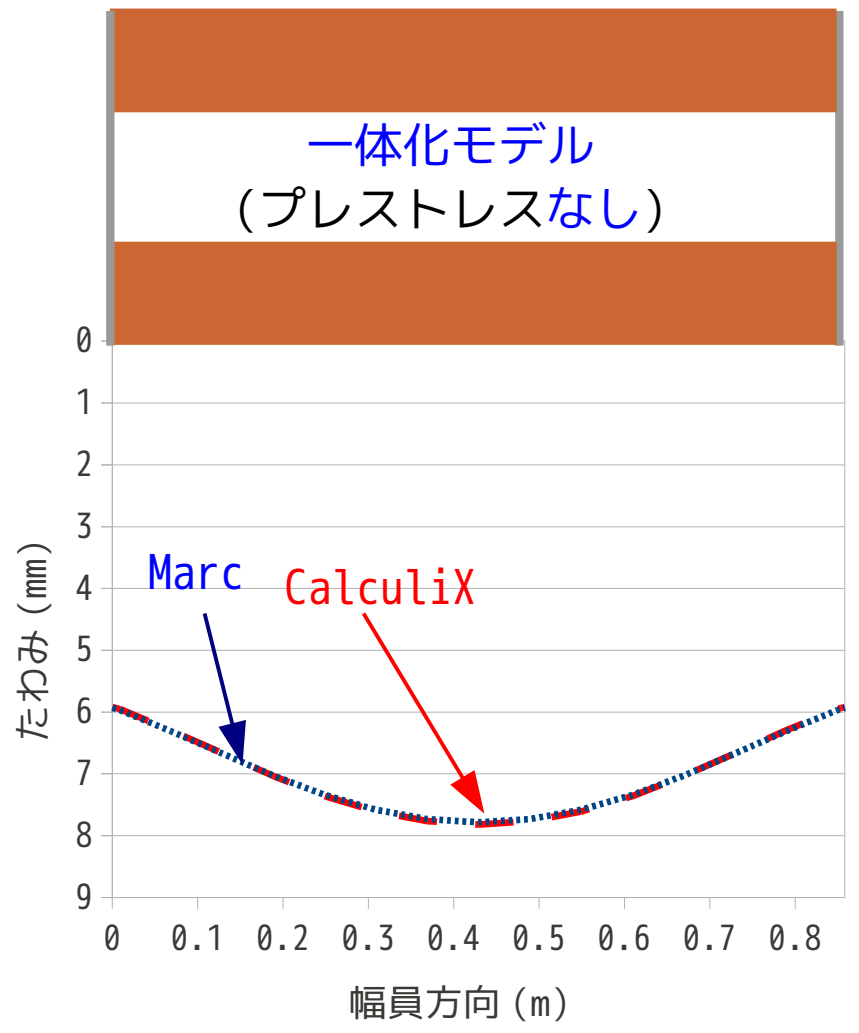
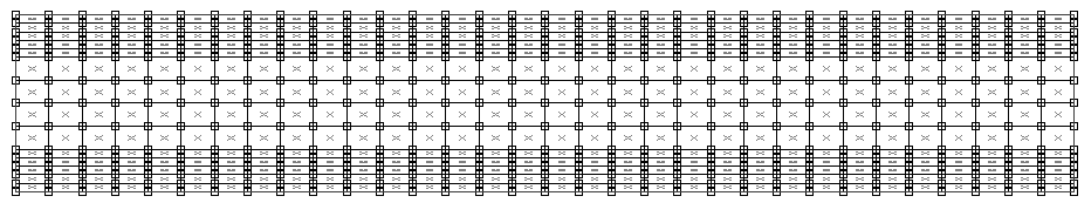
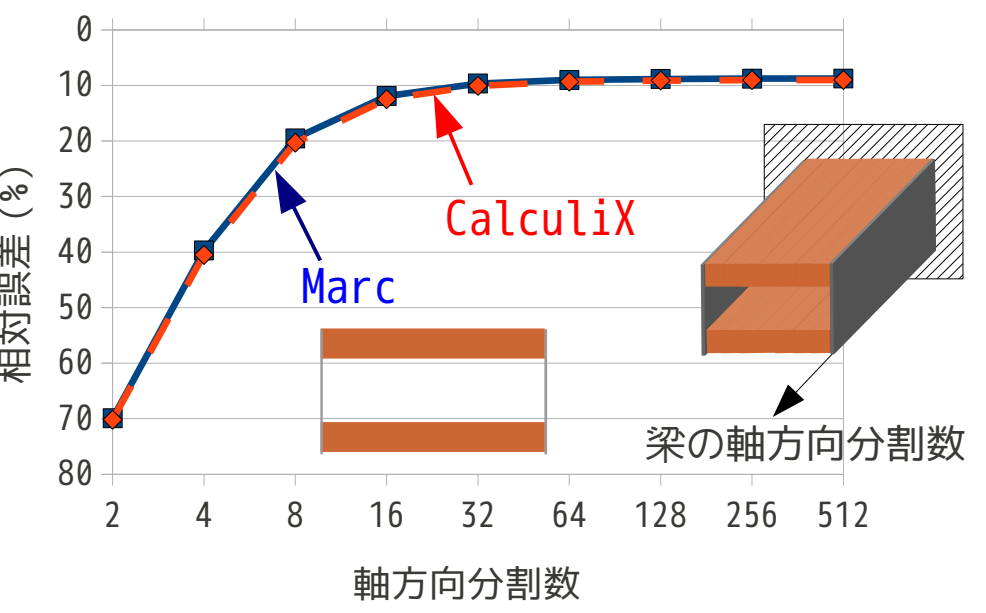
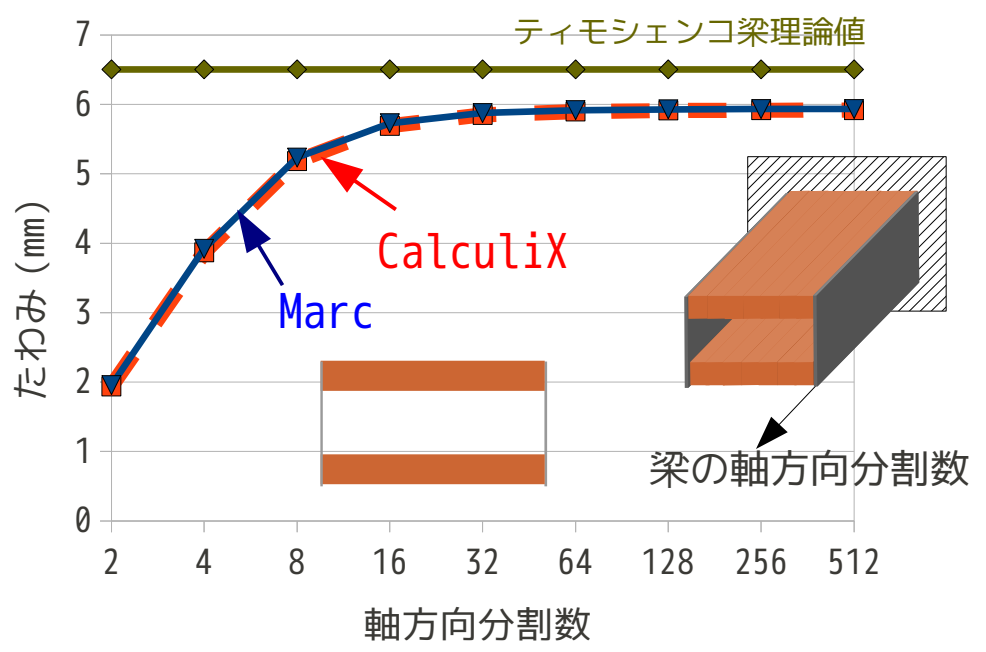
境界条件・载荷条件



50kN
载荷断面の全節点数 → 载荷断面
各節点に一様载荷

非一体化モデルと一体化モデルの比較する前に...

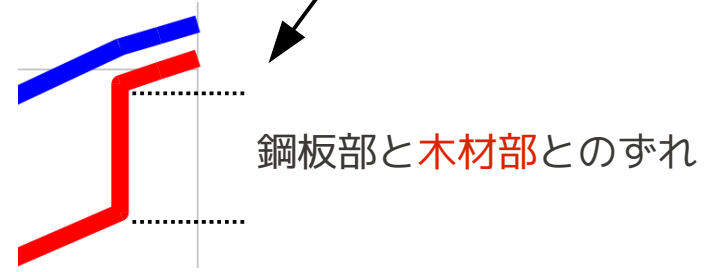
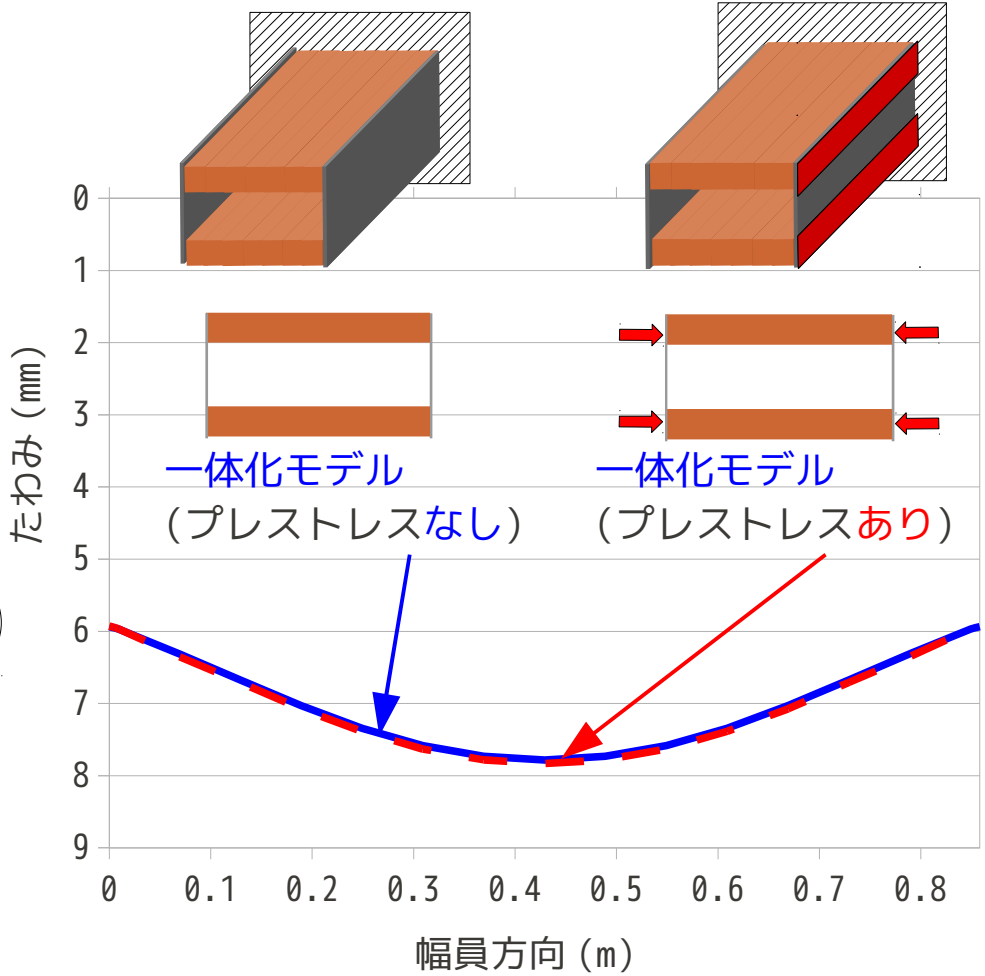
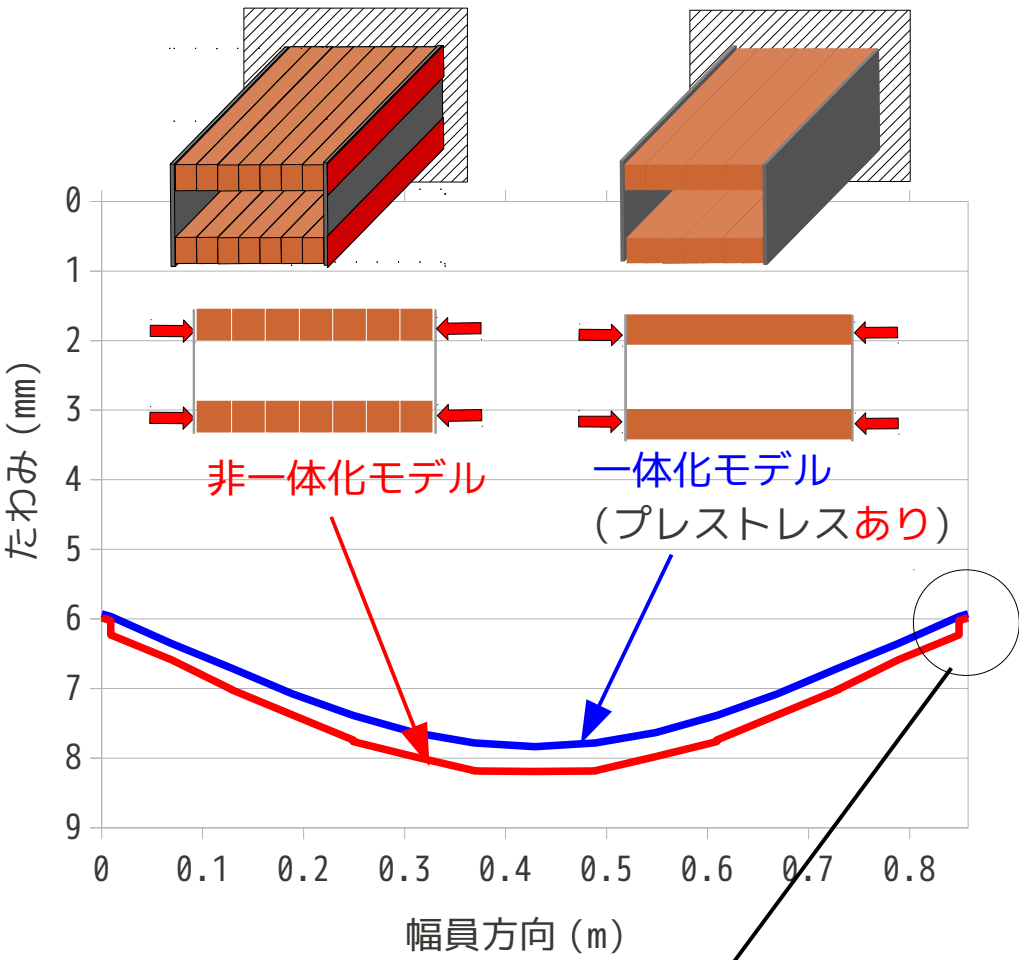
CalculiXとMarcの精度比較



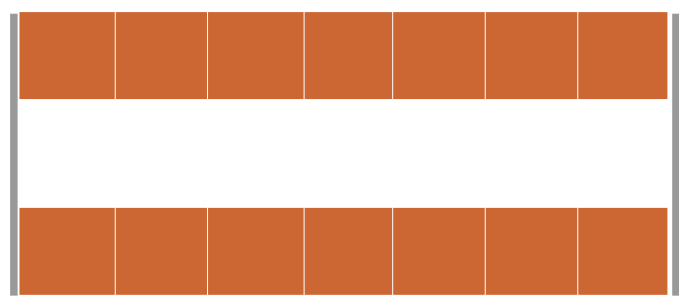
以下、解析はMarcを用いる

たわみと幅員方向の関係

摩擦係数0.4

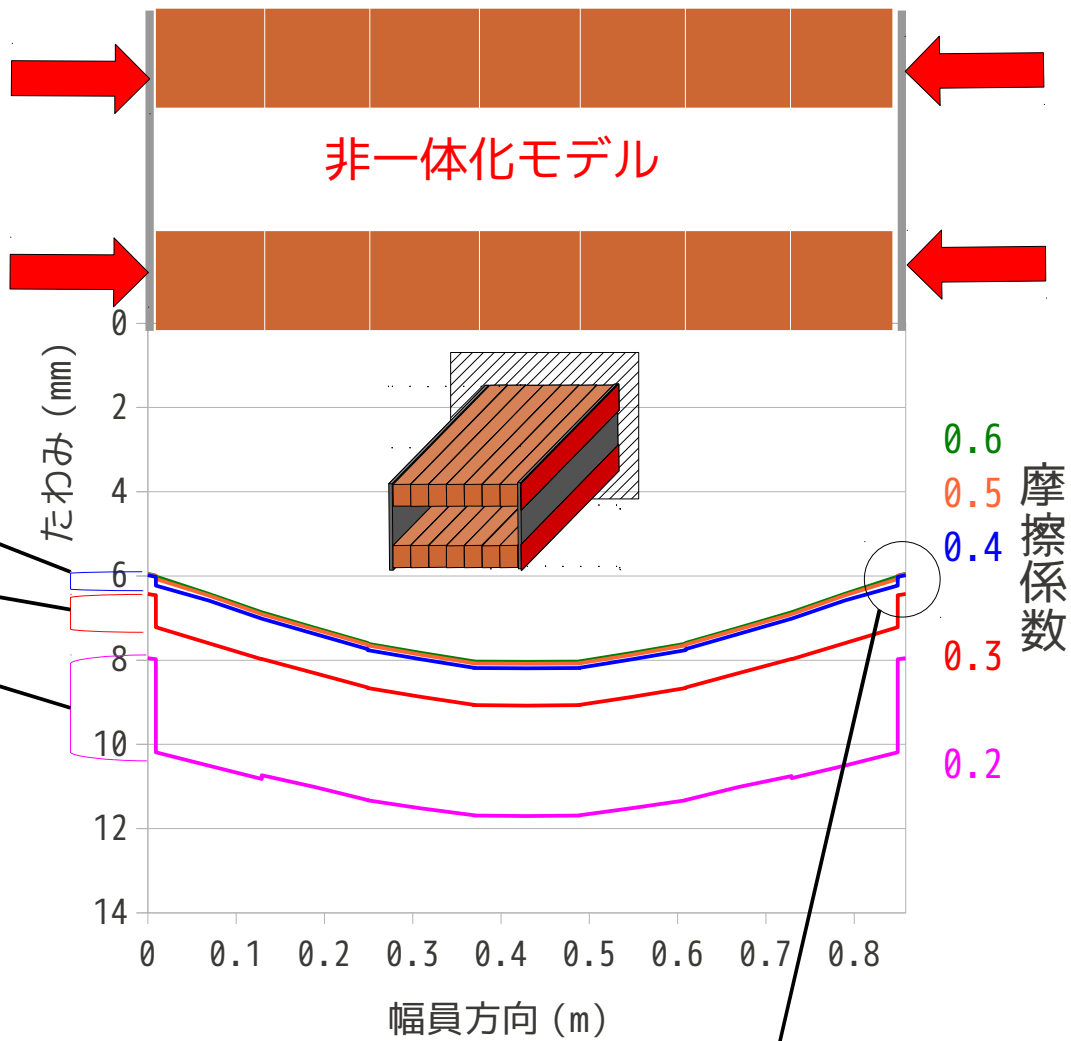


摩擦係数を変化させると...

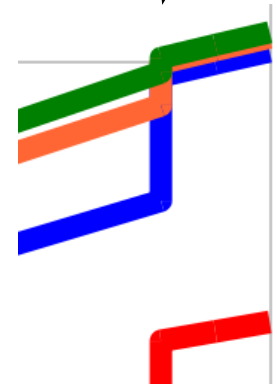


- 異種材料摩擦係数
- 木材と鋼材
→ 0.6(乾)~0.2(湿)
 - 木材と木材
→ 0.5(乾)~0.2(湿)
 - 鋼材と鋼材
→ 0.8(乾)~0.2(湿)

鋼板部と木材部のずれ



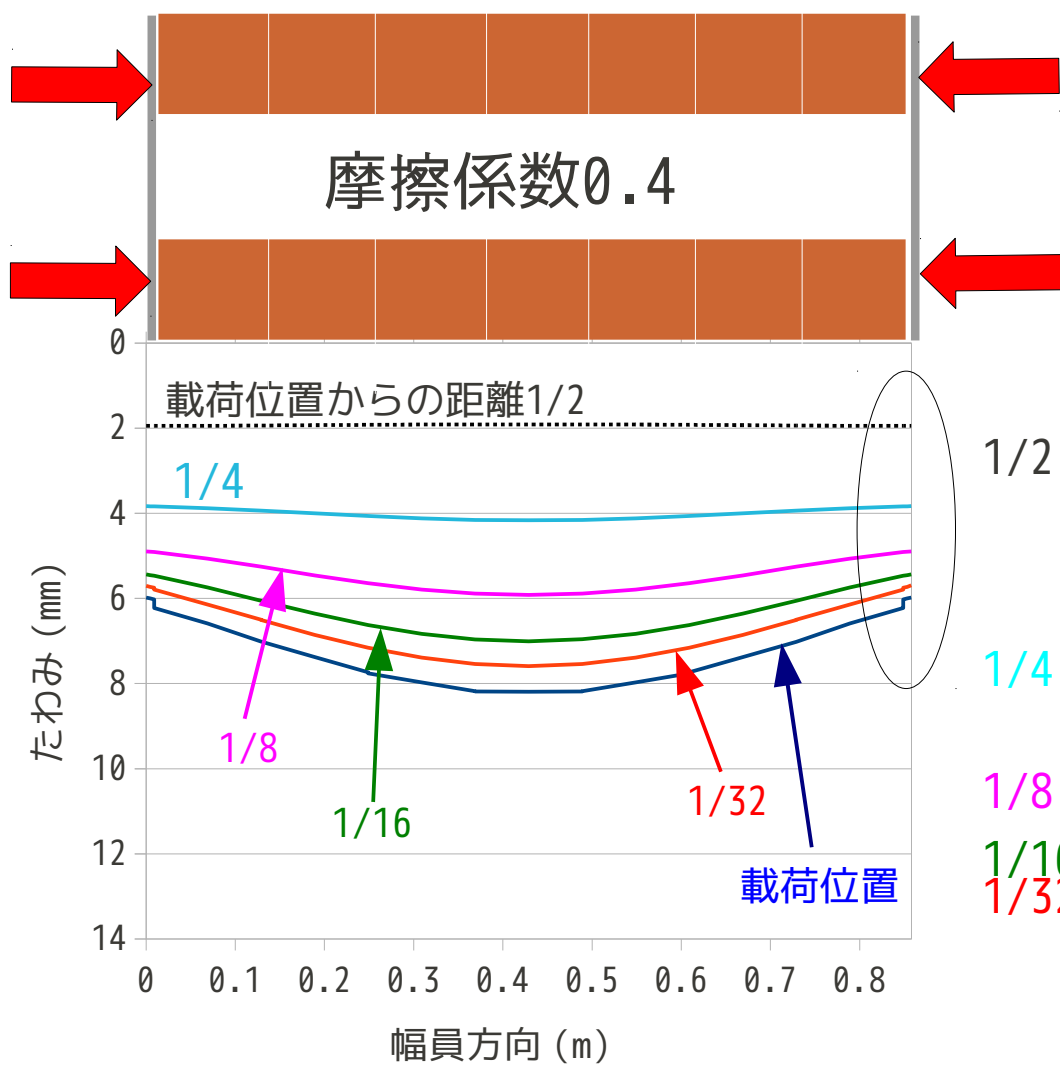
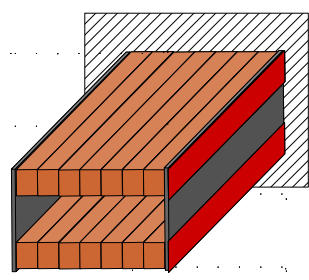
載荷断面からどのように？
全体的に？FEM特有の部分的に？



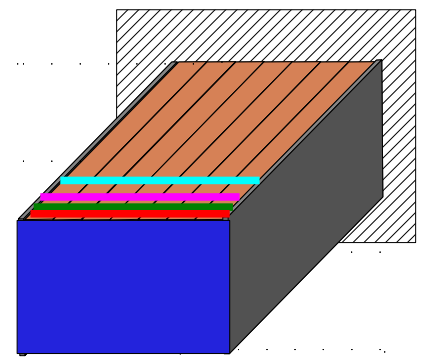
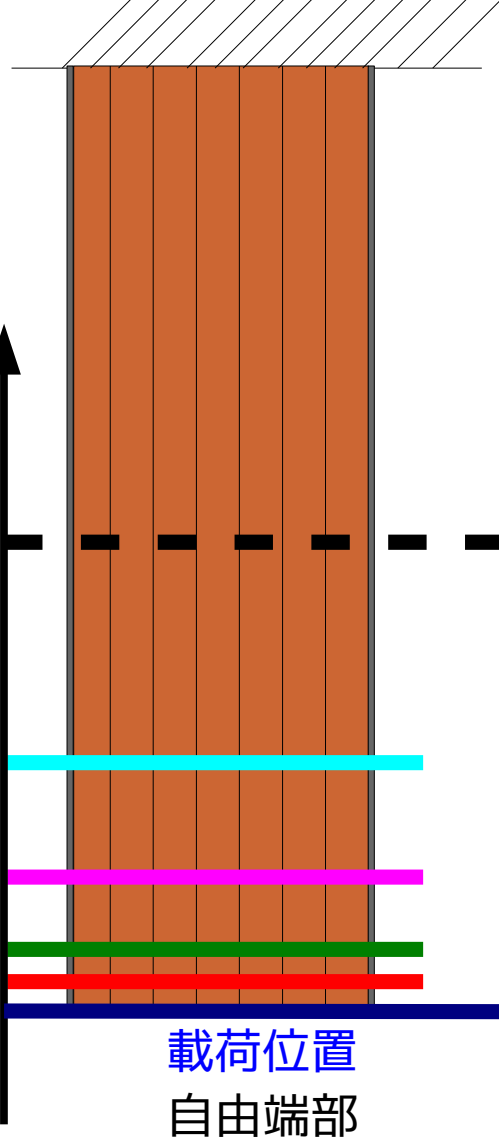
載荷位置からの距離別

たわみと幅員方向の関係

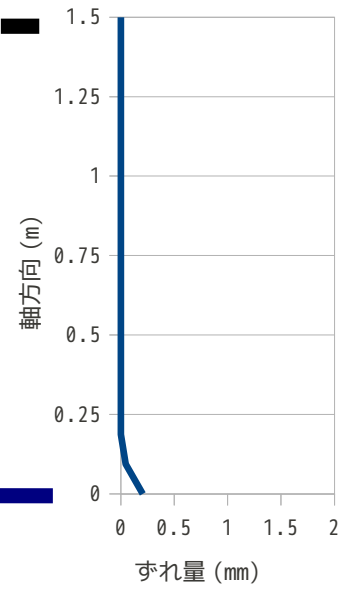
非一体化モデル



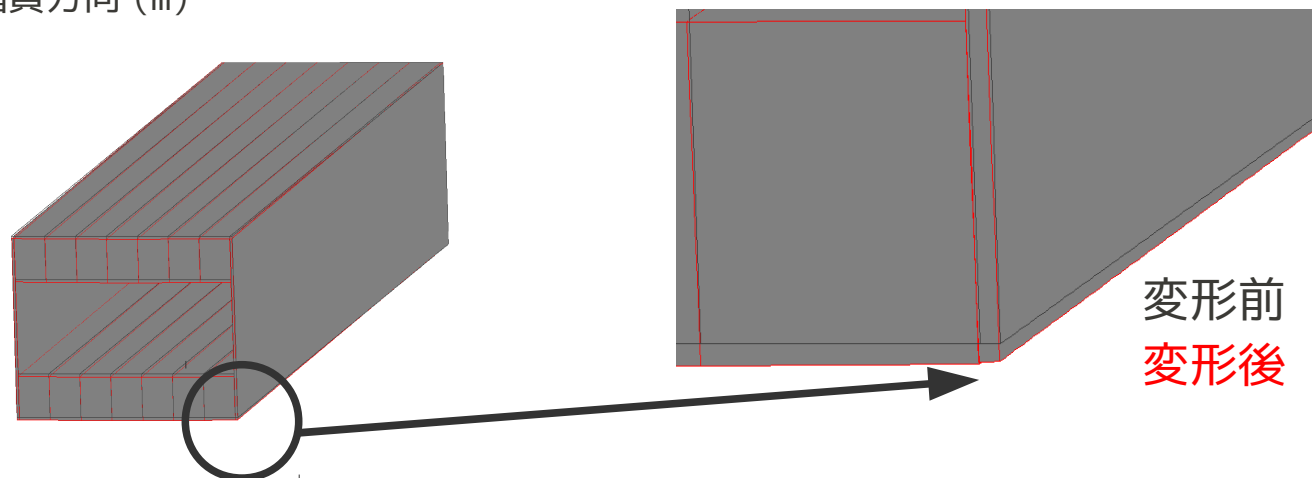
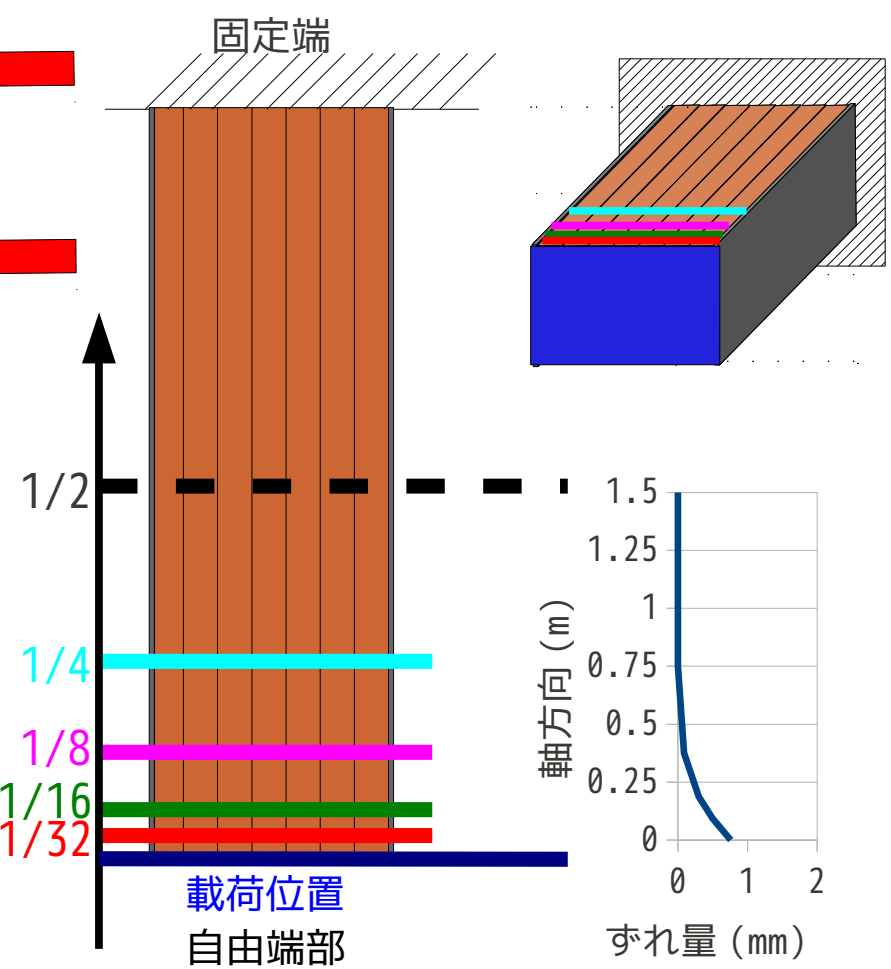
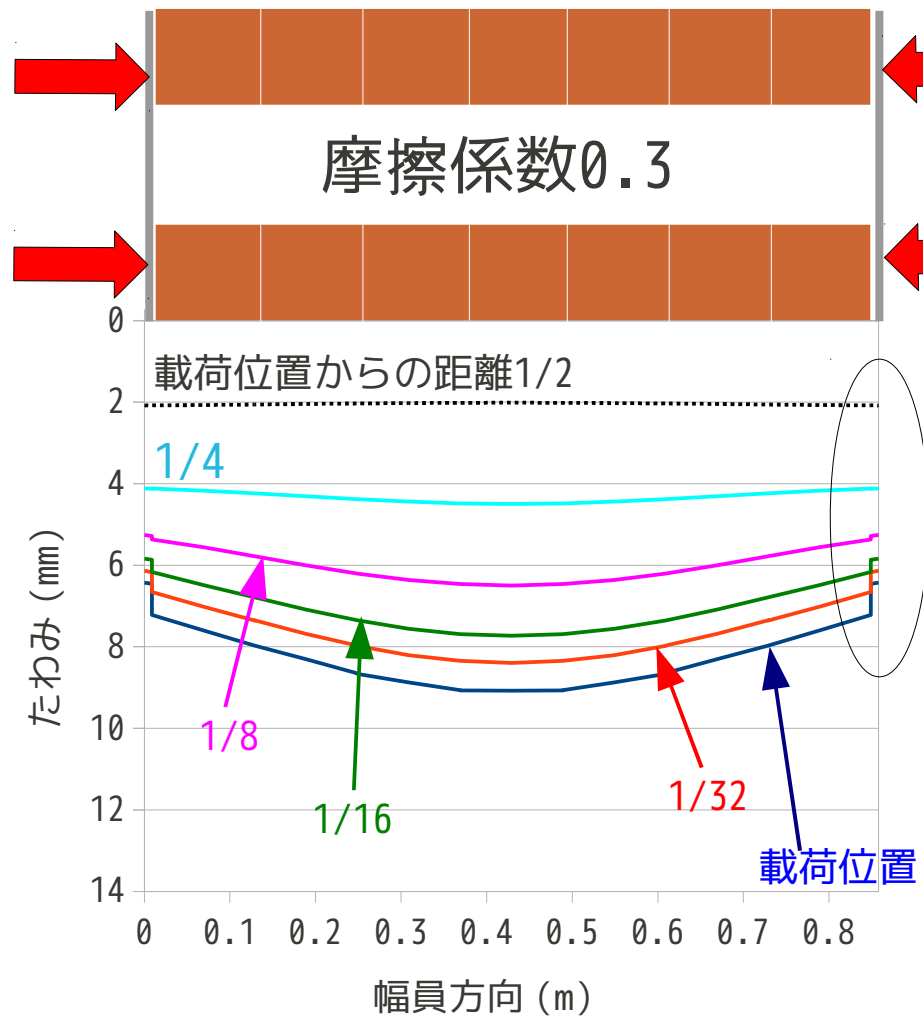
固定端



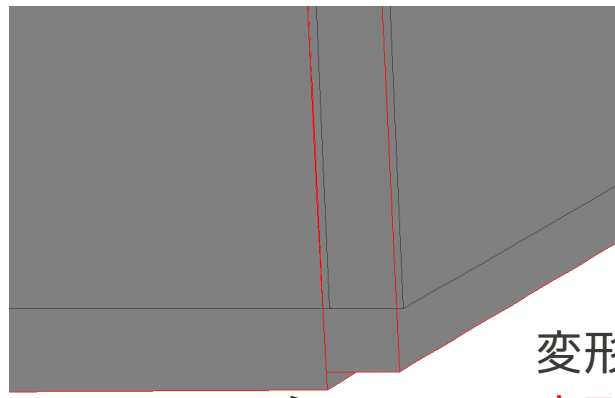
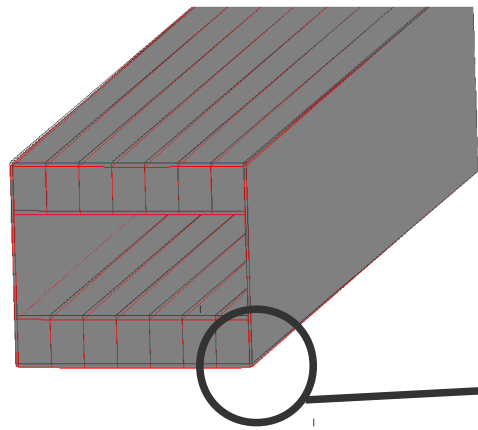
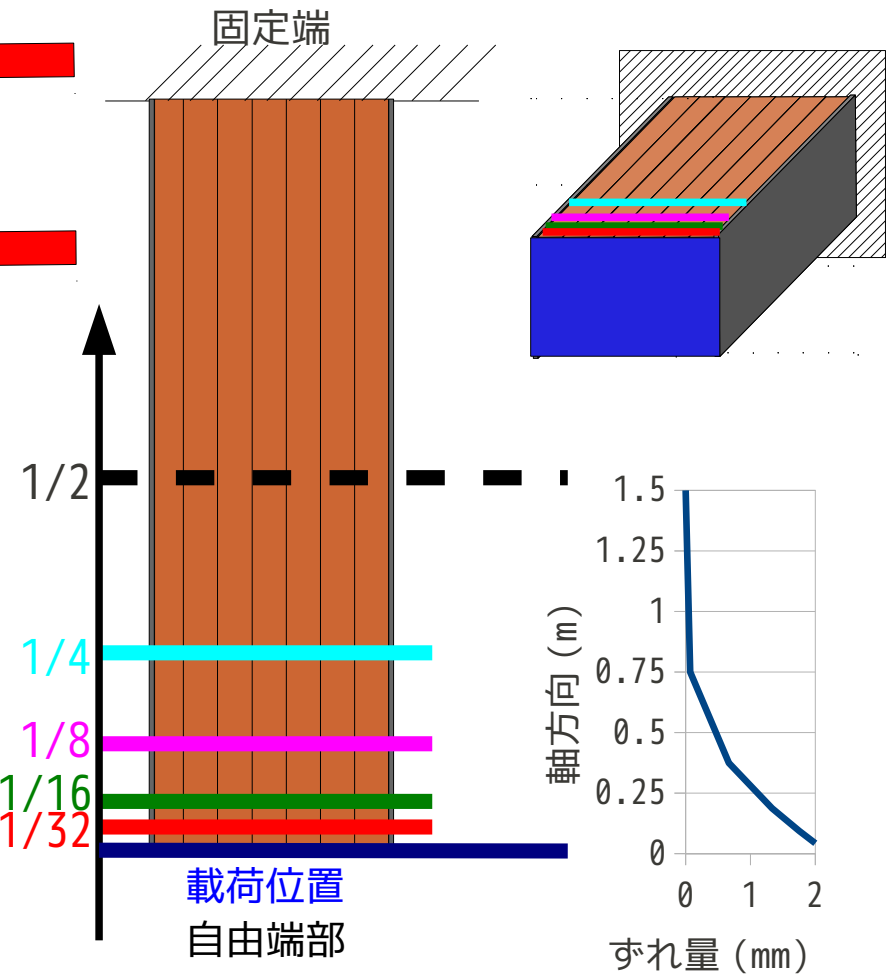
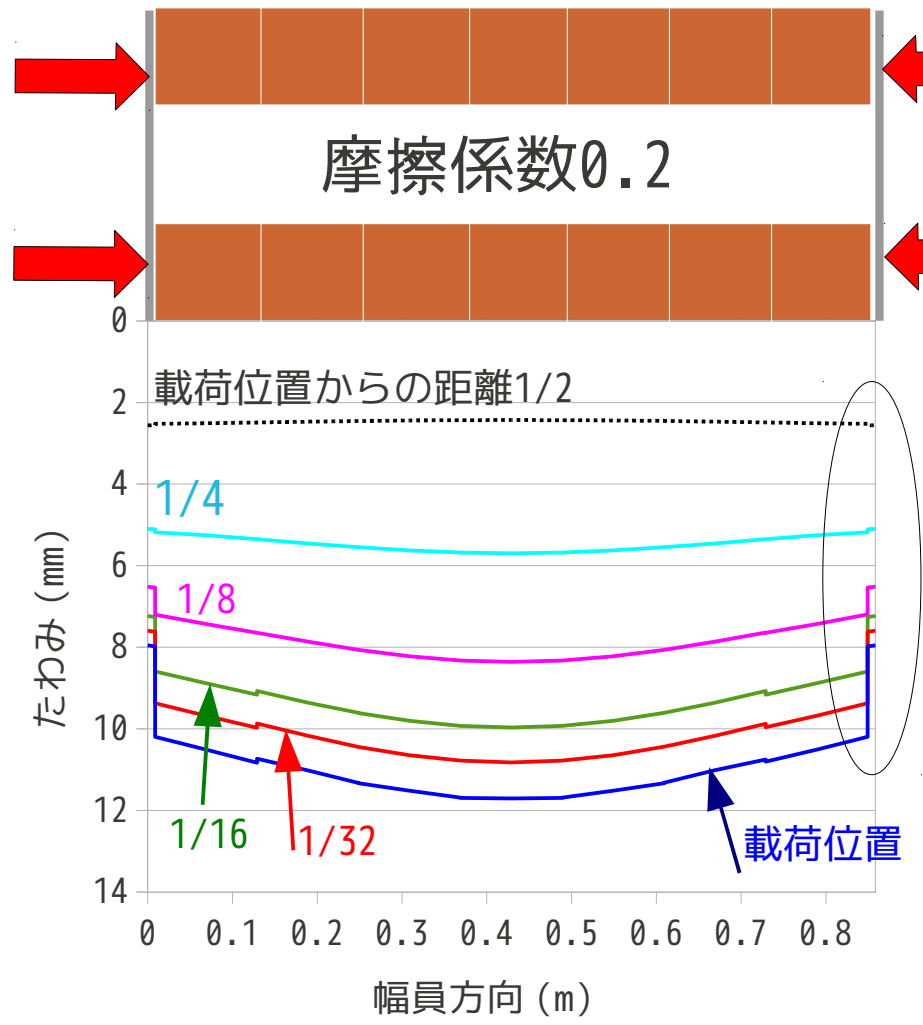
載荷断面



載荷位置からの距離別 たわみと幅員方向の関係

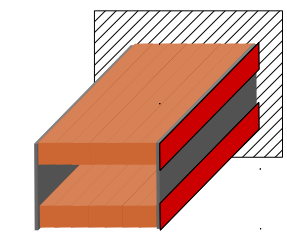


載荷位置からの距離別 たわみと幅員方向の関係

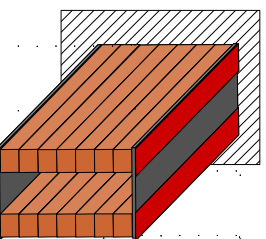


変形前
変形後

FEM解析と実験値の比較



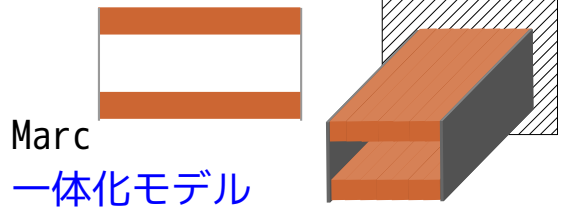
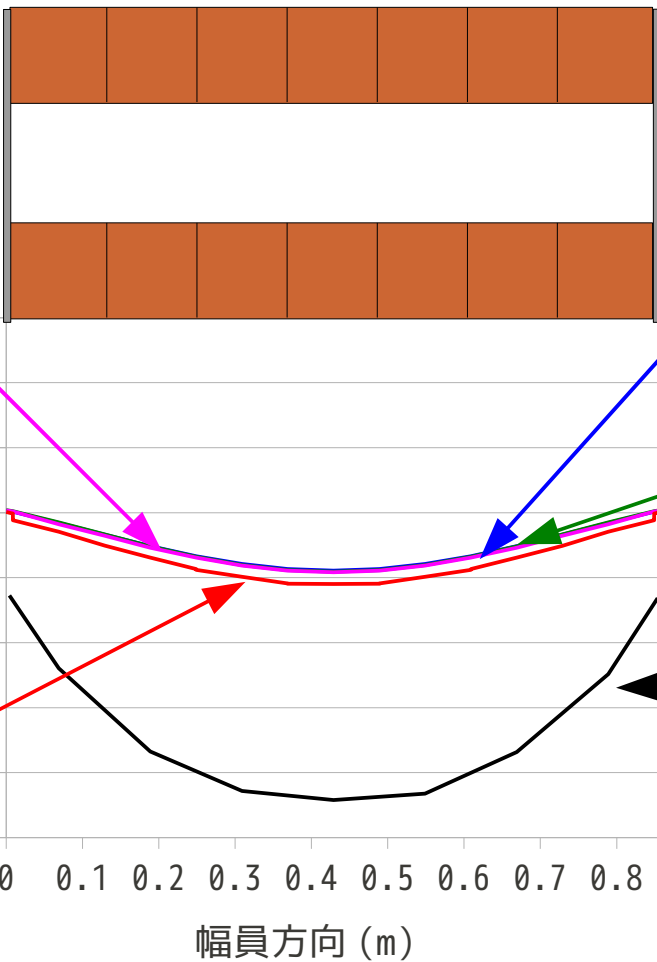
Marc
 一体化モデル
 プレストレスあり



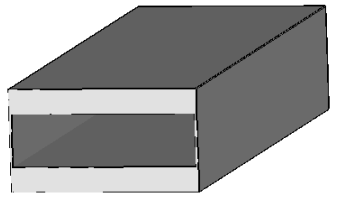
Marc
 非一体化モデル



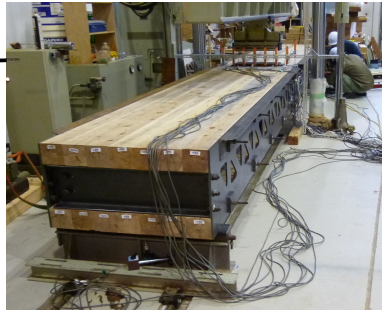
摩擦係数0.4



Marc
 一体化モデル
 プレストレスなし

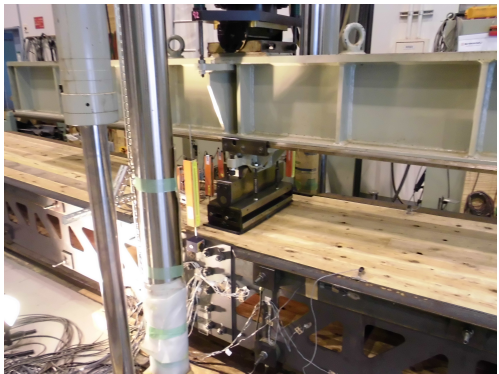
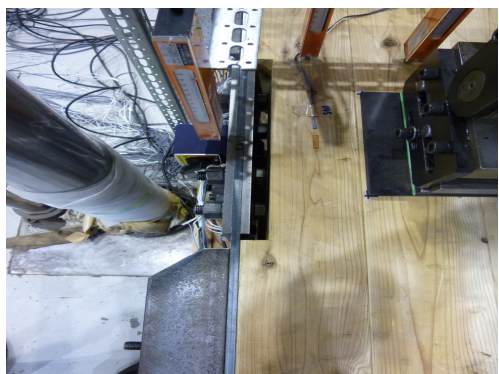


CalculiX

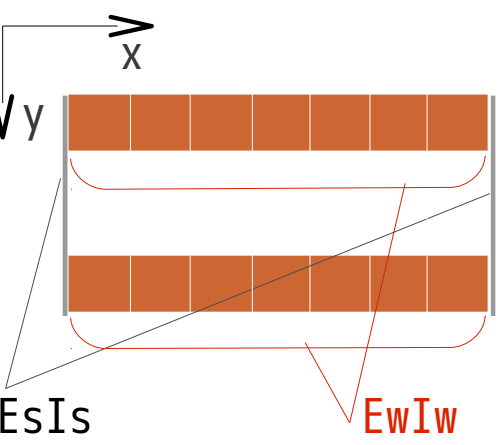


実験値

通常の载荷試験 $\xrightarrow{\text{荷重 2倍}}$ 破壊試験



解析上、ずれを起きにくくしても...



鋼板部と木材部とのずれ

$$EsIs > EwIw$$

剛性比で荷重を配分して載荷

$$\frac{0.61}{\frac{EsIs}{EsIs+EwIw}} \times P$$

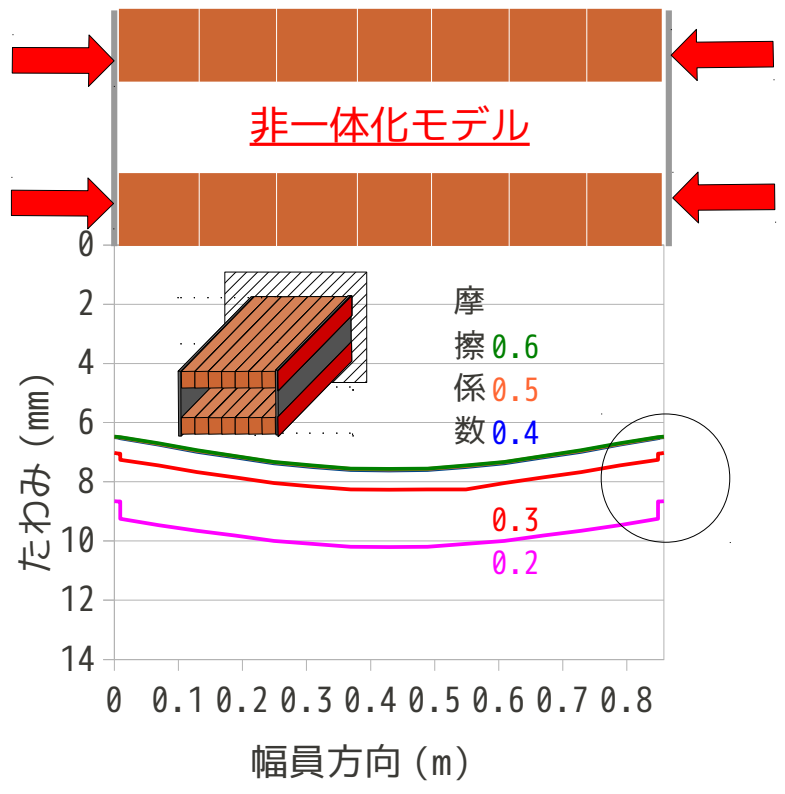
載荷断面の全節点数

→鋼板部の各節点に載荷

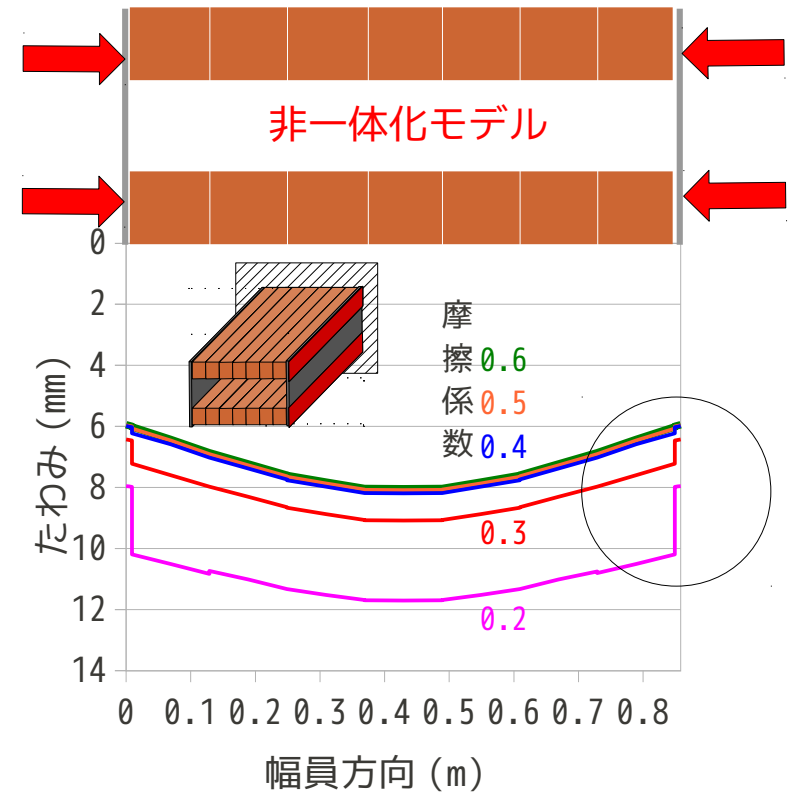
$$\frac{0.39}{\frac{EwIw}{EsIs+EwIw}} \times P$$

載荷断面の全節点数

→木材部の各節点に載荷



一様に載荷



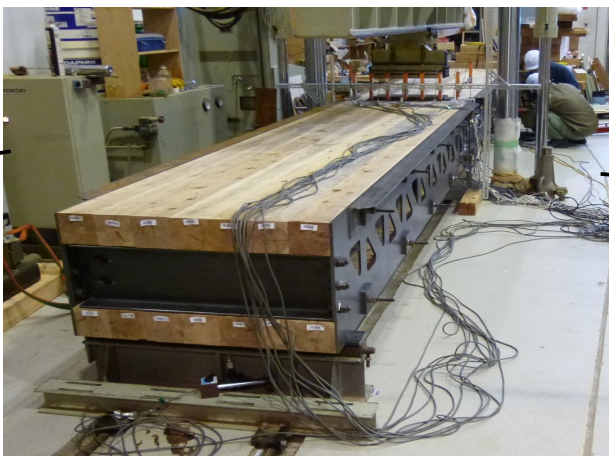
試験体
木材部のみの載荷でも



摩擦係数は十分に大きい

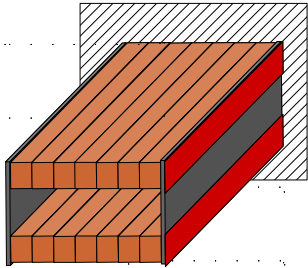
まとめ

試験体



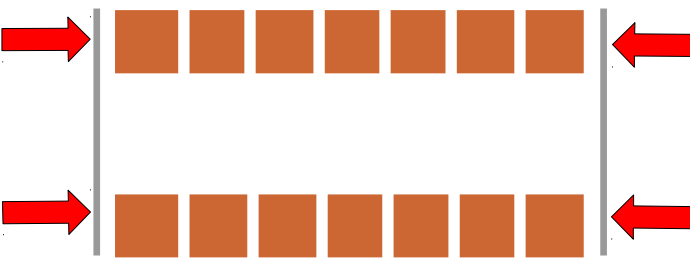
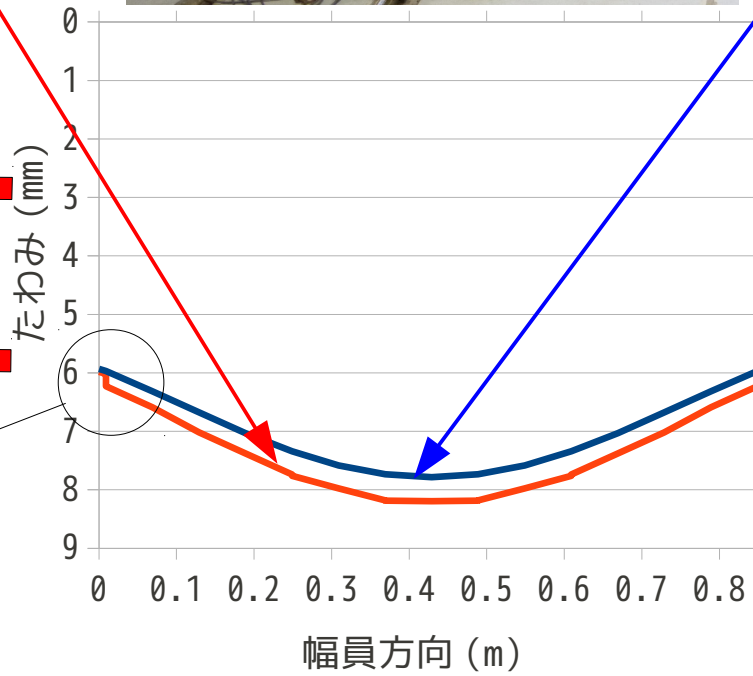
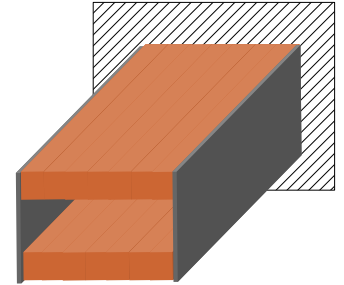
非一体化モデル

モデル化難しい



一体化モデル

モデル化簡単



摩擦係数
0.6 0.5 0.4 0.3 0.2

鋼板と木材にすれ
 $E_s I_s > E_w I_w$

剛性評価可能

プレストレスによる摩擦は十分に大きい

